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# Preliminary Sizing of Large Propeller Driven Aeroplanes

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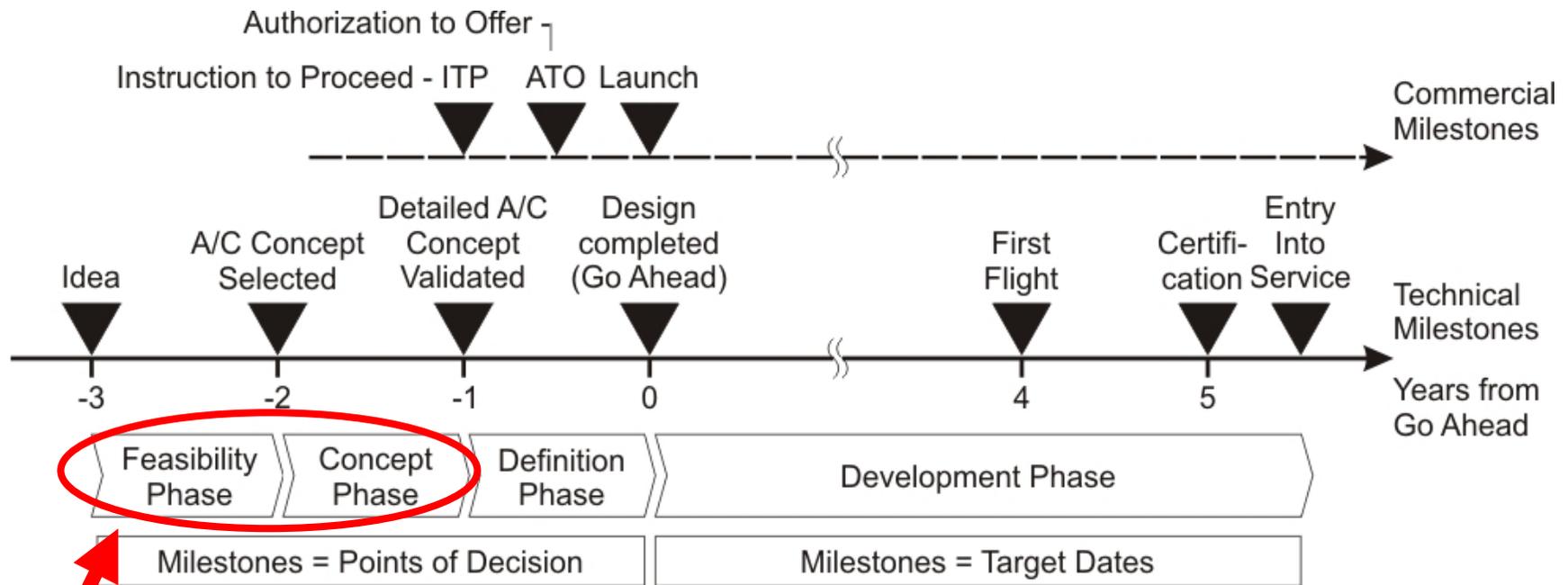
Recent Research and Design Progress in Aeronautical Engineering and its  
Influence on Education

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- **Introduction**
- **Overview**
- **Optimization Parameters from Requirements**
- **Combining Results**
- **Example Calculation: ATR 72**
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# Introduction



**Preliminary Sizing**

## Requirements

- Payload,  $m_{PL}$
- Range,  $R$
- Mach number in cruise,  $M_{CR}$  or speed,  $V_{CR}$
- Take-off field length,  $S_{TOFL}$
- Landing field length,  $S_{LFL}$  or approach speed,  $V_{APP}$   
or stall speed,  $V_S$
- Climb gradient  $\gamma$  during second segment
- Climb gradient  $\gamma$  during missed approach

## Aircraft Parameters

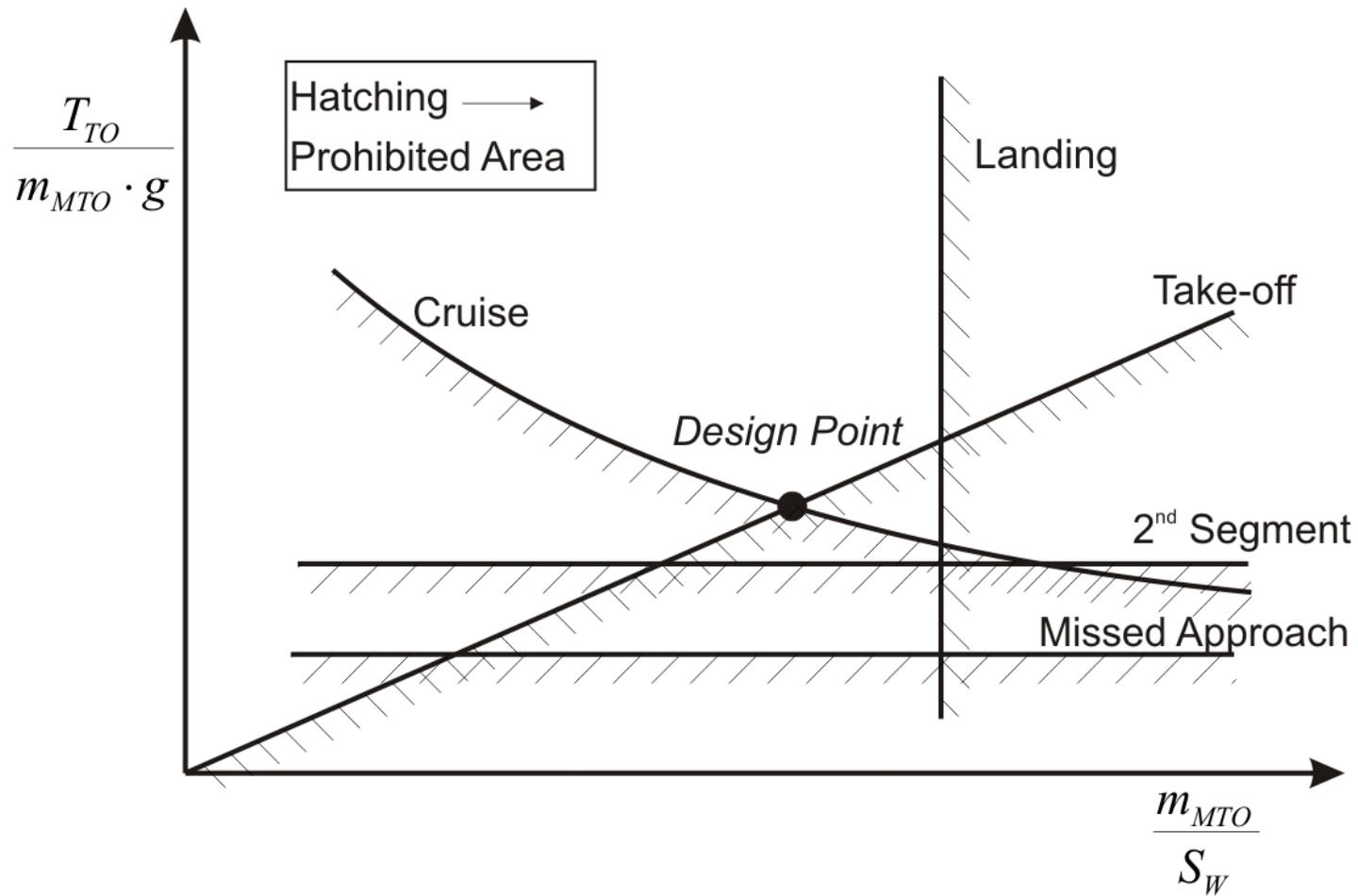
- Take-off mass,  $m_{MTO}$
- Fuel mass,  $m_F$
- Operating empty mass,  $m_{OE}$
- Wing area,  $S_W$
- Take-off thrust,  $T_{TO}$  or take-off power,  $P_{TO}$

# Introduction

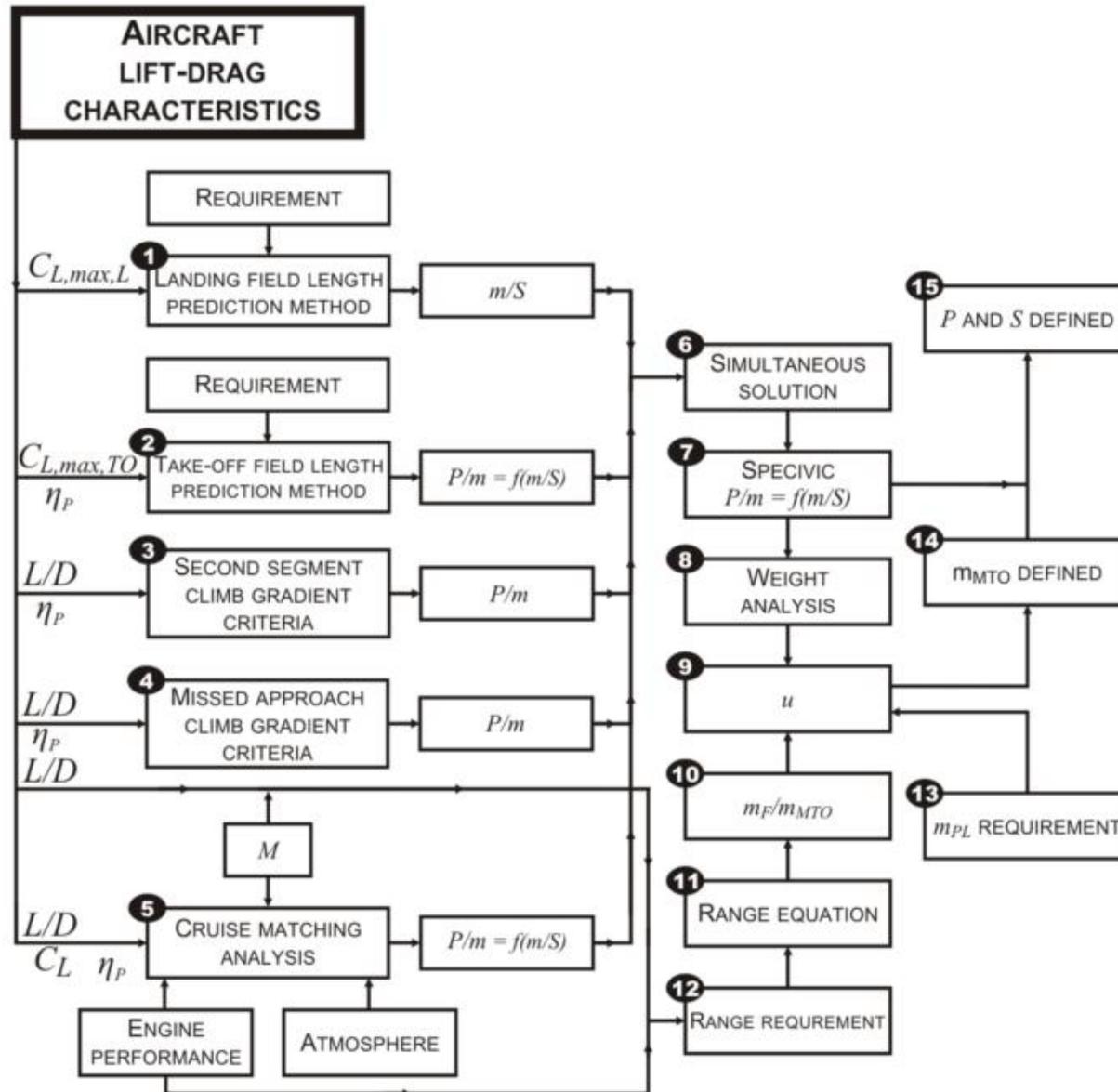
## Aeroplane Categories, Propulsion System and Certification Rules

1. **large jet aeroplanes** are certified to CS-25 respectively FAR Part 25,
2. **very light jets** are certified to CS-23 respectively FAR Part 23,
3. **large propeller driven aeroplanes** are also certified to CS-25 respectively FAR Part 25
4. **smaller propeller driven aeroplanes** (normal, utility, aerobatic and commuter aeroplanes) are certified to CS-23 respectively FAR Part 23,
5. **very light propeller driven aeroplanes** (up to a maximum take-off mass of 750 kg) can be certified to CS-VLA,
6. different certification rules exist for **ultra light aircraft**.

## General Approach



# Overview



# Optimization Parameters from Requirements



## Optimization Parameters

- Power to mass ratio  $\frac{P_{TO}}{m_{MTO}}$
- Wing loading  $\frac{m_{MTO}}{S_W}$
- The requirements are specified for the various phases of flight ....

## Approach Speed

The landing requirements can be stated in terms of approach speed or landing field length.

One can be converted into the other:  $S_{LFL} = \left( \frac{V_{APP}}{k_{APP}} \right)^2$

$k_{APP} = 1.93 \sqrt{\frac{\text{m}}{\text{s}^2}}$  Statistical factor for large turboprop aircraft  
(calculated from  $k_L$ )

or

$$k_{APP} = \sqrt{\frac{2g \cdot 1.3^2}{\rho_0}} k_L = 5.20 \sqrt{k_L}$$

# Optimization Parameters from Requirements



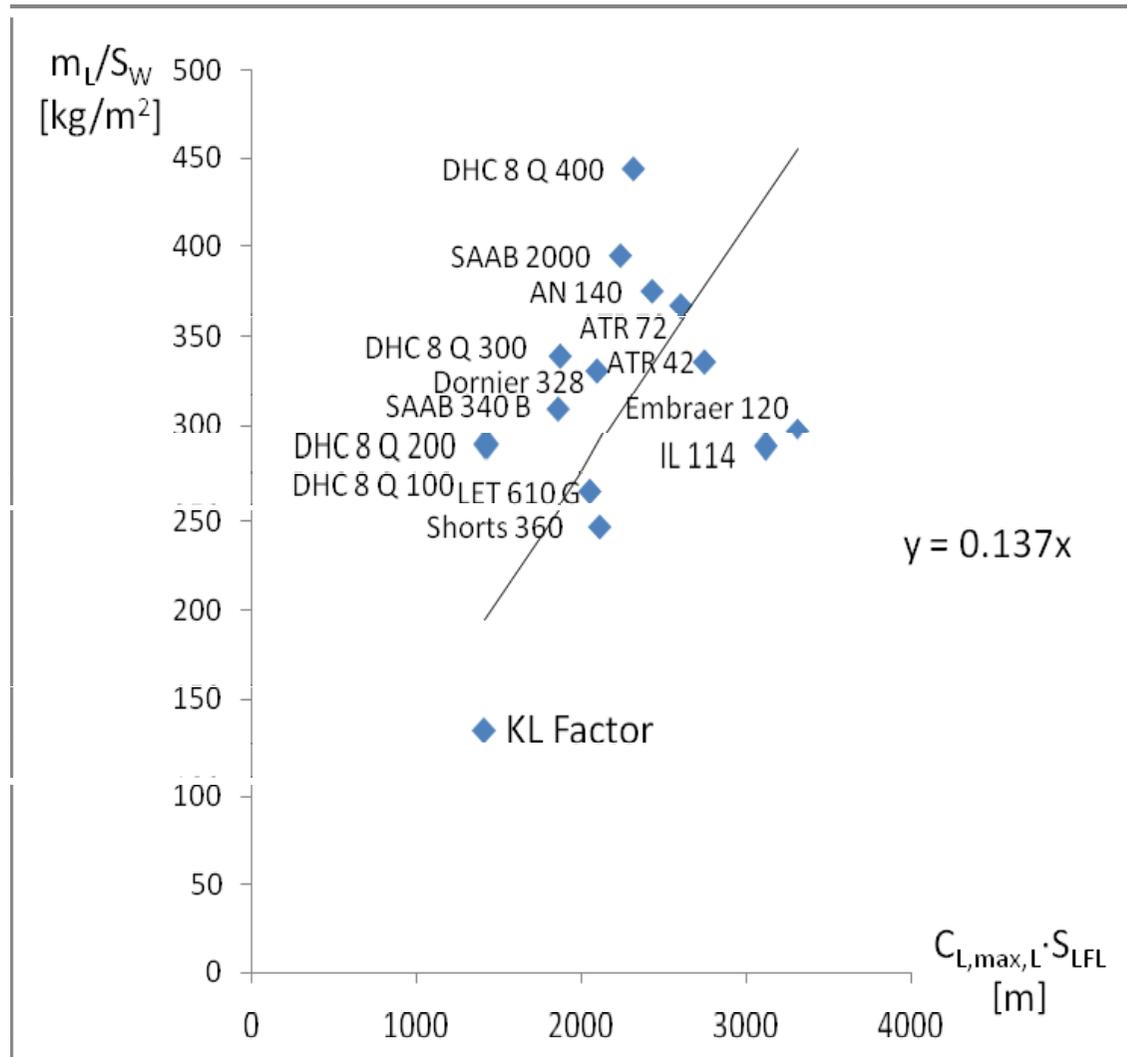
## Landing Field Length

$$m_{MTO} / S_W \leq \frac{k_L \cdot \sigma \cdot C_{L,max,L} \cdot S_{LFL}}{m_{ML} / m_{MTO}}$$

# Optimization Parameters from Requirements



## Landing Field Length



$$k_L = 0.137 \frac{\text{kg}}{\text{m}^3}$$

Statistical  
factor for  
large  
turboprop  
aircrafts

# Optimization Parameters from Requirements



## Take-Off Field Length

$$\frac{P_{TO} / m_{MTO}}{m_{MTO} / S_W} \geq \frac{k_{TO} \cdot V \cdot g}{S_{TOFL} \cdot \sigma \cdot C_{L,max,TO} \cdot \eta_{P,TO}}$$

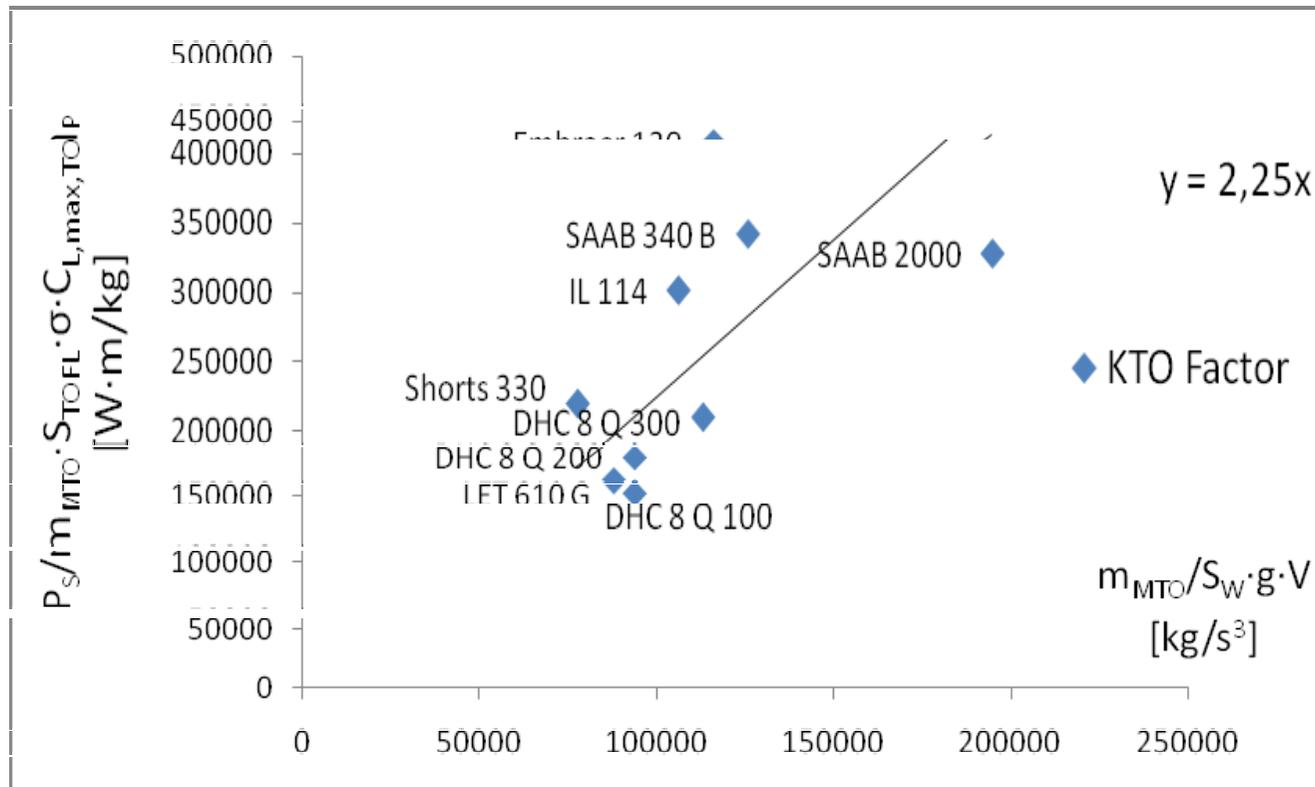
# Optimization Parameters from Requirements



## Take-Off Field Length

$$k_{TO} = 2.25 \frac{\text{m}^3}{\text{kg}}$$

Statistical factor for large turboprop aircrafts



# Optimization Parameters from Requirements



## Take-Off Field Length

$$V = V_2 / \sqrt{2}$$

$$V_2 = 1.2 V_{S,TO}$$

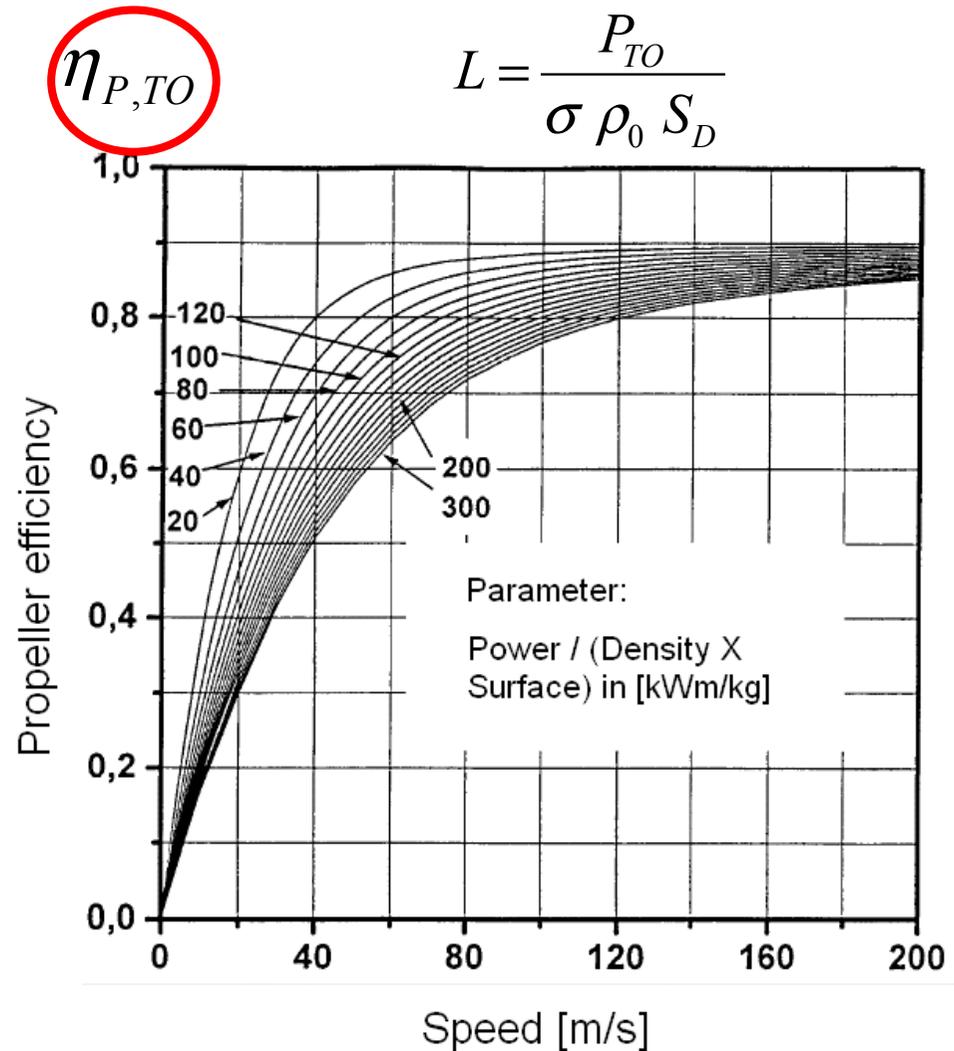
$$V_{S,TO} = V_{S,L} \sqrt{\frac{C_{L,max}}{C_{TO,max}}}$$

$$V_{S,L} = V_{APP} / 1.3$$

$$\sigma = \frac{\rho}{\rho_0} = \frac{288.15 \text{ K}}{288.15 \text{ K} + \Delta \vartheta_{TO}}$$

disc loading

$$L = \frac{P_{TO}}{\sigma \rho_0 S_D}$$



# Optimization Parameters from Requirements



## Climb Rate during 2nd Segment

$$\frac{P_{TO}}{m_{MTO}} \geq \frac{n_E}{n_E - 1} \cdot \left( \frac{1}{E} + \sin \gamma \right) \cdot \left( \frac{V_2 \cdot g}{\eta_{P,CL}} \right)$$

$$E = \frac{C_L}{C_D} = \frac{C_L}{C_{D,P} + \frac{C_L^2}{\pi \cdot A \cdot e}} \quad C_L = \frac{C_{L,max,TO}}{1.2^2} \quad e = 0.7$$

$$C_{D,P} = 0.05C_L - 0.035$$

$$C_L \geq 1.1$$

$C_L$  depends on flap settings

# Optimization Parameters from Requirements



## Climb Rate during Missed Approach

$$\frac{P_{TO}}{m_{MTO}} \geq \frac{n_E}{n_E - 1} \cdot \left( \frac{1}{E} + \sin \gamma \right) \cdot \left( \frac{V_{APP} \cdot g}{\eta_{P,L}} \right) \cdot \left( \frac{m_{ML}}{m_{MTO}} \right)$$

$$E = \frac{C_L}{C_D} = \frac{C_L}{C_{D,P} + \frac{C_L^2}{\pi \cdot A \cdot e}}$$

$\frac{C_{L,max,L}}{1.3^2}$   
 $e = 0.7$

$$C_{D,P} = 0.05C_L - 0.035 + \Delta C_{D,gear}$$

$$C_L \geq 1.1$$

$C_L$  depends on flap settings

# Optimization Parameters from Requirements



## Cruise

Lift = Weight

$$\frac{m_{MTO}}{S_W} = \frac{C_L \cdot M_{CR}^2}{g} \cdot \frac{\gamma}{2} \cdot p(H) \quad \text{or} \quad \frac{m_{MTO}}{S_W} = \frac{C_L \cdot \rho_0 \cdot V_{CR}^2 \cdot \sigma(H)}{2 \cdot g}$$

$$C_L = \frac{C_{L,md}}{(V/V_{md})^2} \quad \text{with} \quad C_{L,md} = \frac{\pi A e}{2 E_{\max}}$$

# Optimization Parameters from Requirements



## Cruise

Drag = Thrust

$$\frac{P_{TO}}{m_{MTO}} = \frac{M_{CR} \cdot a(H) \cdot g}{P_{CR} / P_{TO} \cdot E \cdot \eta_{P,CR}}$$

or

$$\frac{P_{TO}}{m_{MTO}} = \frac{V_{CR} \cdot g}{P_{CR} / P_{TO} \cdot E \cdot \eta_{P,CR}}$$

$$E = \frac{2E_{\max}}{\frac{1}{\left(\frac{C_L}{C_{L,md}}\right)} + \left(\frac{C_L}{C_{L,md}}\right)}$$

with

$$C_L / C_{L,md} = 1 / (V / V_{md})^2$$

# Optimization Parameters from Requirements

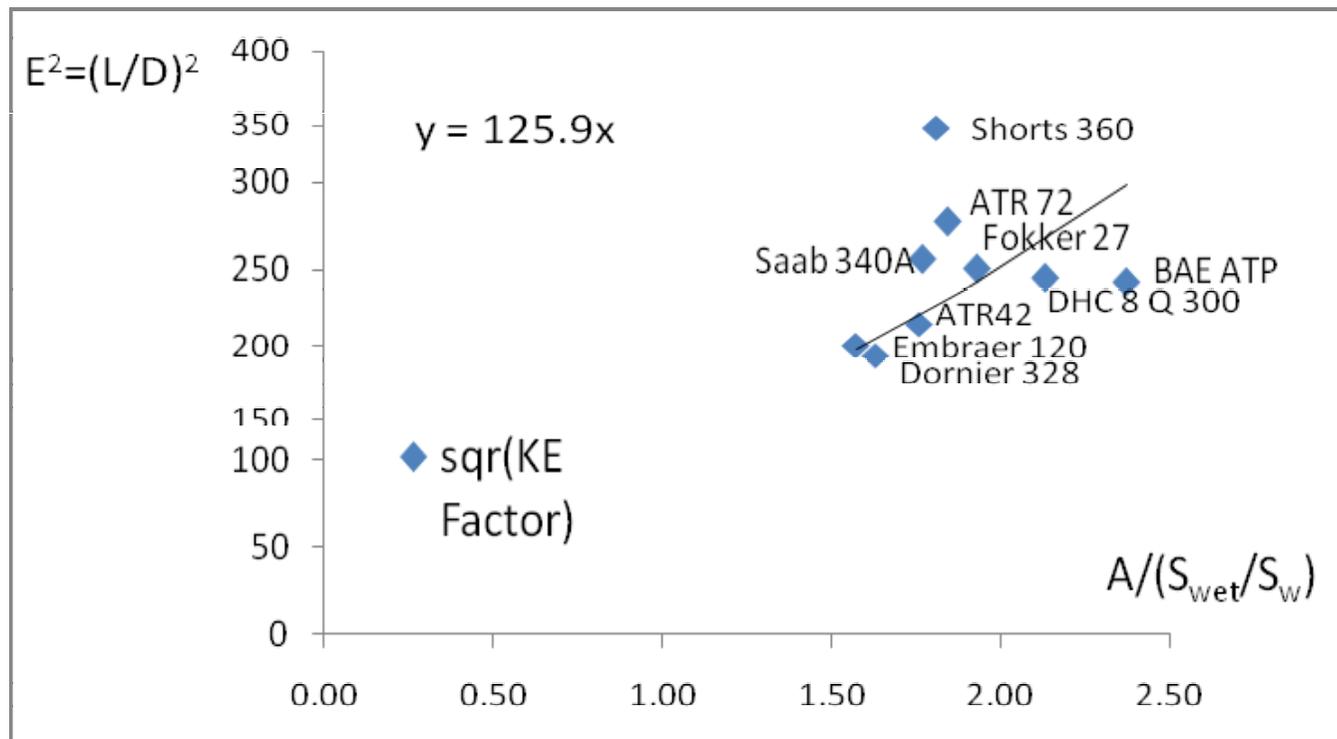


## Cruise

### Maximum Glide Ratio Estimation

$$E_{\max} = k_E \cdot \sqrt{\frac{A}{S_{wet} / S_W}} \quad k_E = 11.22$$

Statistical factor for large turboprop aircrafts



# Optimization Parameters from Requirements



## Cruise

### Engine Power Estimation

$$P / P_0 = AM^m \sigma^n \quad \text{for turboprop engines}$$

Author	Ref.Nr.	Page	Engine	$A$	$m$	$n$
Schaufele	[14]	187	generic	1.036	0.101	0.851
Brüning	[15]	58	T 64-GE-7	1.121	0.168	0.755
Russel	[16]	16	Rolls-Royce	1.725	0.267	0.966
Loftin	[7]	375	generic	1.089	0.091	0.924
McCormick & Barnes	[17]	351	PW 120	1.883	0.740	0.929
Average				1.371	0.273	0.885

# Combining Results



1) Generation of **matching chart** from optimization parameters

$$m_{MTO} = \frac{m_{PL}}{1 - \frac{m_F}{m_{MTO}} - \frac{m_{OE}}{m_{MTO}}}$$

2) Estimation of relative **operating empty mass**

$$\frac{m_{LOI}}{m_{CR}} = e^{-\frac{s_{CR}}{B_s}}$$

$$B_s = \frac{E \cdot \eta_P}{SFC \cdot g}$$

3) Calculation of relative **fuel mass** using fuel fractions. Additional distance for flight to an alternate (200 NM) and loiter time 45 min.

# Example Calculation: ATR 72

## Requirements

Landing:  $S_{LFL} = 1067 \text{ m}$

Take off:  $S_{TOFL} = 1290 \text{ m}$

2<sup>nd</sup> Segment:  $n_E = 2 \quad \sin \gamma = 0.024$

Missed Approach:  $n_E = 2 \quad \sin \gamma = 0.021$

Cruise:  $M = 0.41$

Range:  $R = 715 \text{ NM}$

Payload:  $m_{PL} = 6460 \text{ kg}$

# Example Calculation: ATR 72

## Results

### Aerodynamics and Propeller Efficiency

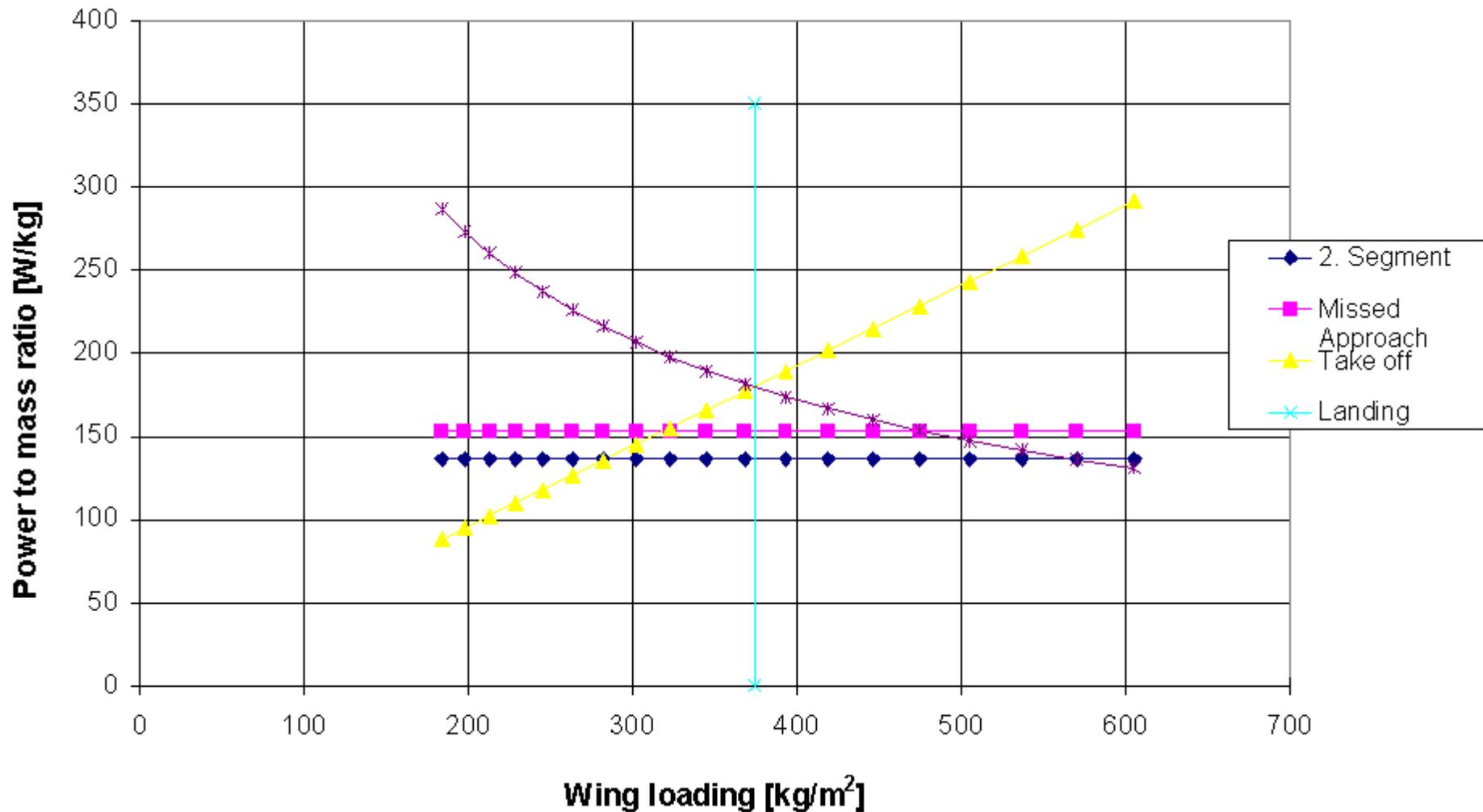
Flight Phase	$C_{L,max}$	$C_L$	$E_{max}$	$E$	$\eta_P$
Landing	2.5				
Take-off	2.1				0.64
2 <sup>nd</sup> Segment		1.46		12.28	0.73
Missed Approach		1.48		10.79	0.73
Cruise		0.503	15.74	12.49	0.86

# Example Calculation: ATR 72



## Results

### Matching Chart



# Example Calculation: ATR 72



## Results

### Aircraft Parameters

Parameter	Original ATR 72	Redesigned ATR 72	Difference
$m_{MTO}$ [kg]	22800	22925	0.5%
$m_L$ [kg]	22350	22466	0.5%
$m_{OE}$ [kg]	12950	13021	0.5%
$S_W$ [m <sup>2</sup> ]	61	61.35	0.6%
$b$ [m]	27.05	27.13	0.3%
$P_{TO}$ (one engine) [kW]	2051	2061	0.5%
$m_{MTO}/S_W$ [kg/m <sup>2</sup> ]	373.8	373.7	0.0%
$P_{TO}/m_{MTO}$ [W/kg]	179.9	179.8	-0.1%

# Conclusions



- A **preliminary sizing** method for turboprop aeroplanes was presented.
- The method includes – where necessary – equations based on aircraft **statistics**.
- The preliminary sizing method was successfully tested with a **redesign** task of an **ATR 72**.



For further information see  
<http://FE.ProfScholz.de>