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# **Modern Trends in Airframe Structural Design**

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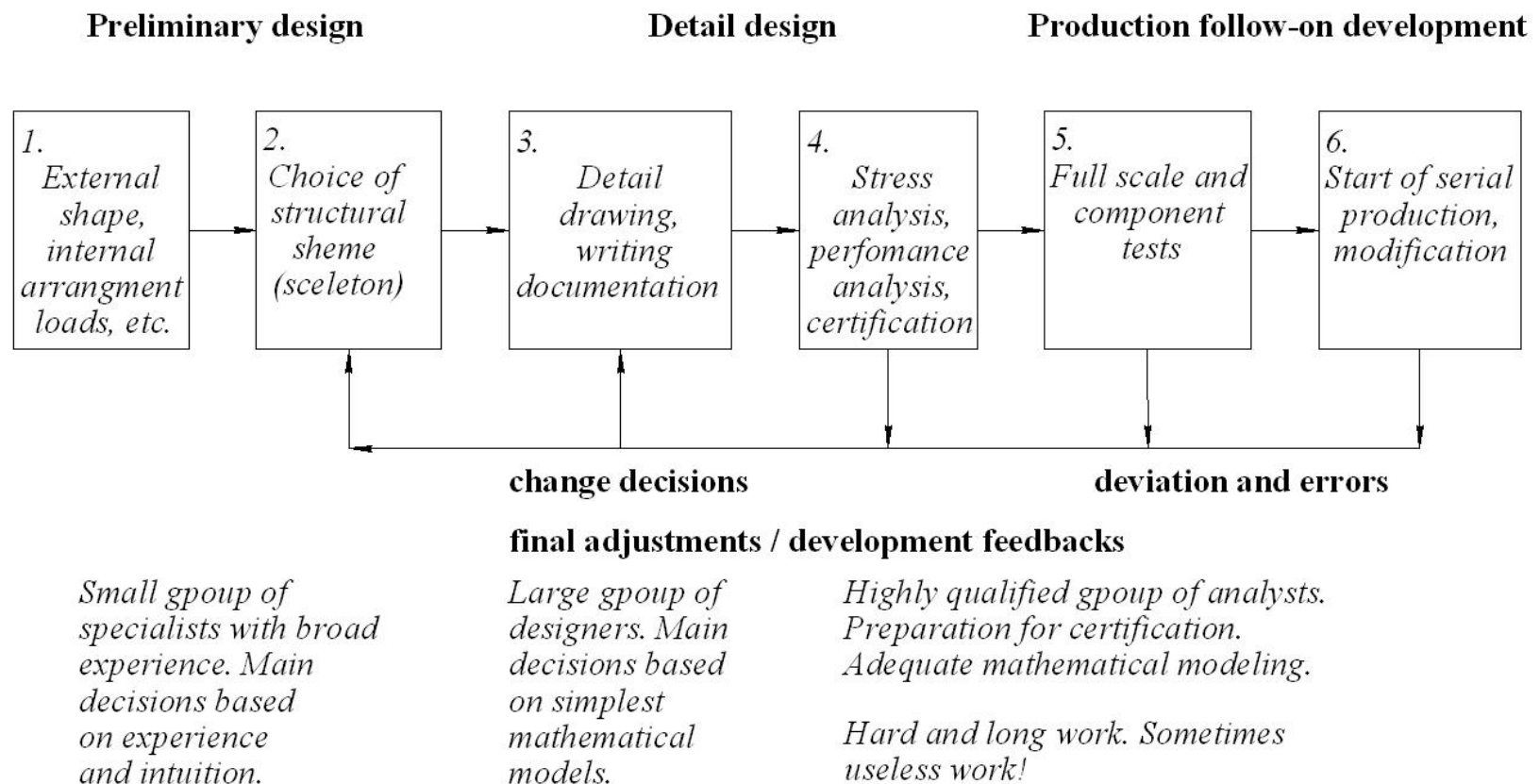
## Plan of the presentation

1. General view on the modern structural design problems.
2. New ideas for improving design process.
3. The example of using a new ideas for research aerodynamic and weight efficiency of morphing wing.

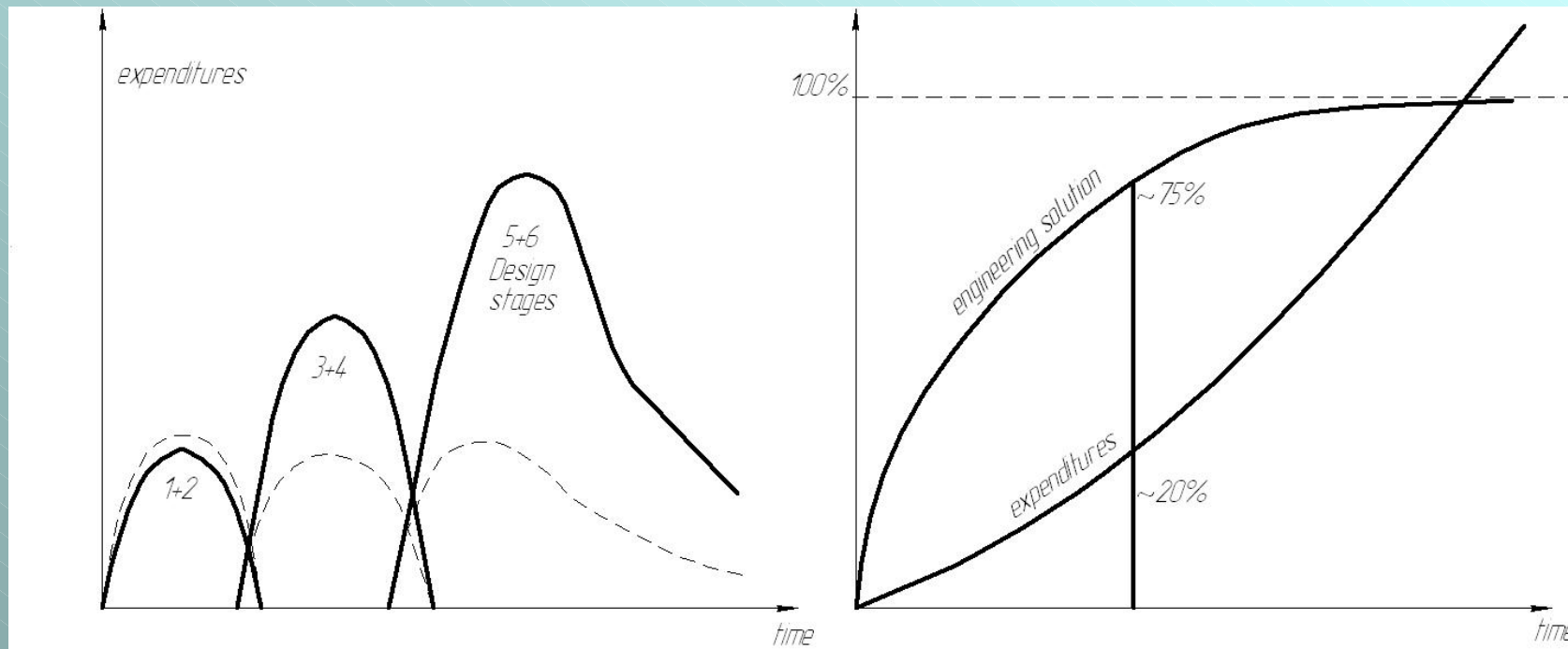


# Airframe design process

## Sequential design paradigm



## Time and resource expenditure



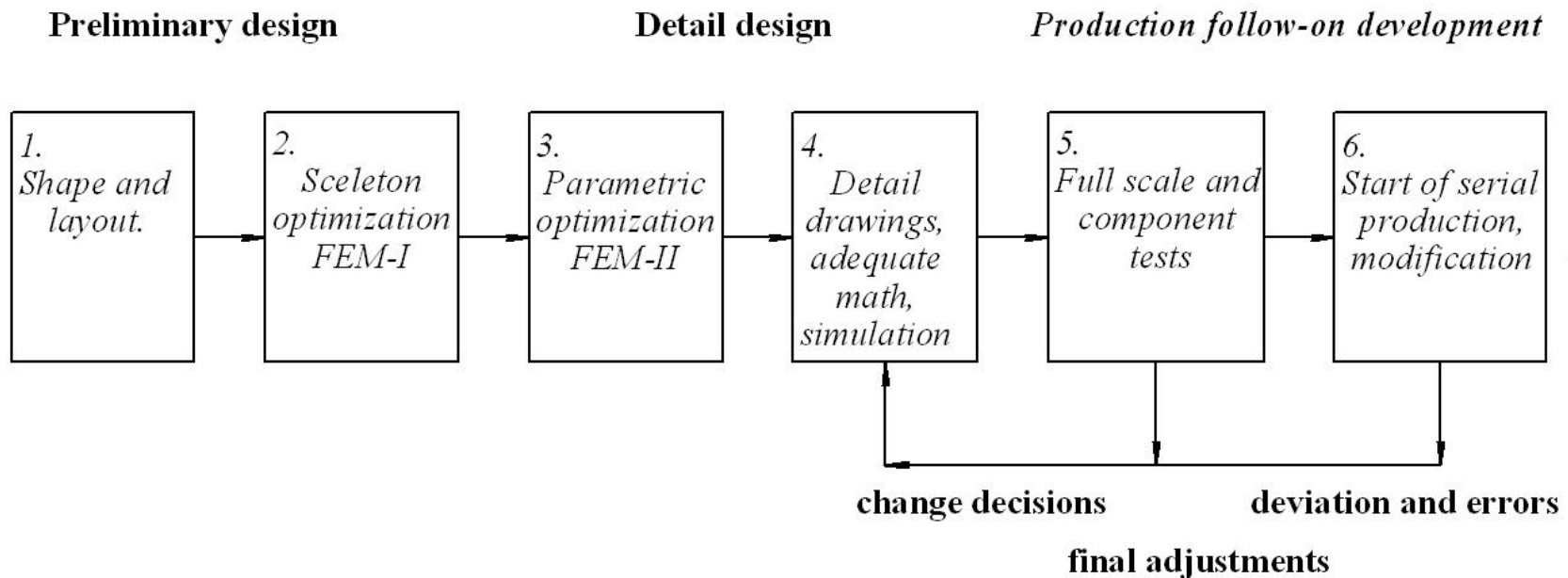
The main reason of greater charges of time and resources in sequential design paradigm is use very simple, (insufficiently exact) mathematical models on early stage of design.

For reduction of designing time it is suitable use of highly accuracy mathematical models on early stage design.



# New paradigm for Airframe Structure Design

## Concurrent design paradigm



*Small group of specialists and specialized software.*

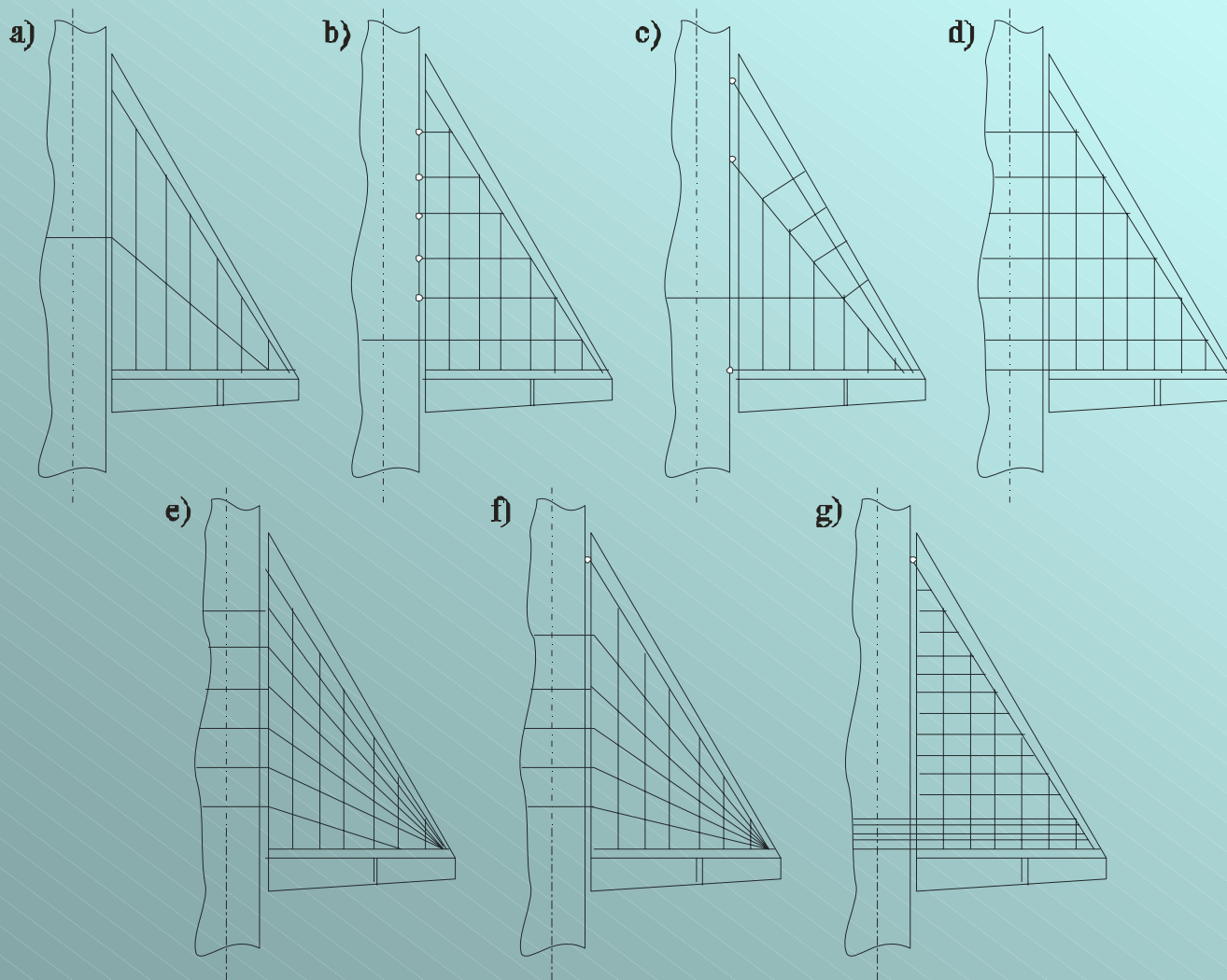
*Analysts and designers work together.  
Amount of mistakes less.  
Time of change decisions is short because we have had mathematical models for adequate analysis of any problems.*



## **The problem of weight estimation in structural design**

1. Choice of structure topology (skeleton design).
2. Estimation of structural mass fraction.
3. Weight estimation of the wing, fuselage, etc.
4. Weight check.

## Choice of structure topology





## Estimation of structural mass fraction

Definition of flight vehicles takeoff gross weight via “equation of existence”

$$m_o = \frac{m_{pl}}{1 - \bar{m}_{st} - \bar{m}_{sys} - \bar{m}_f - \bar{m}_{pp}}$$

where

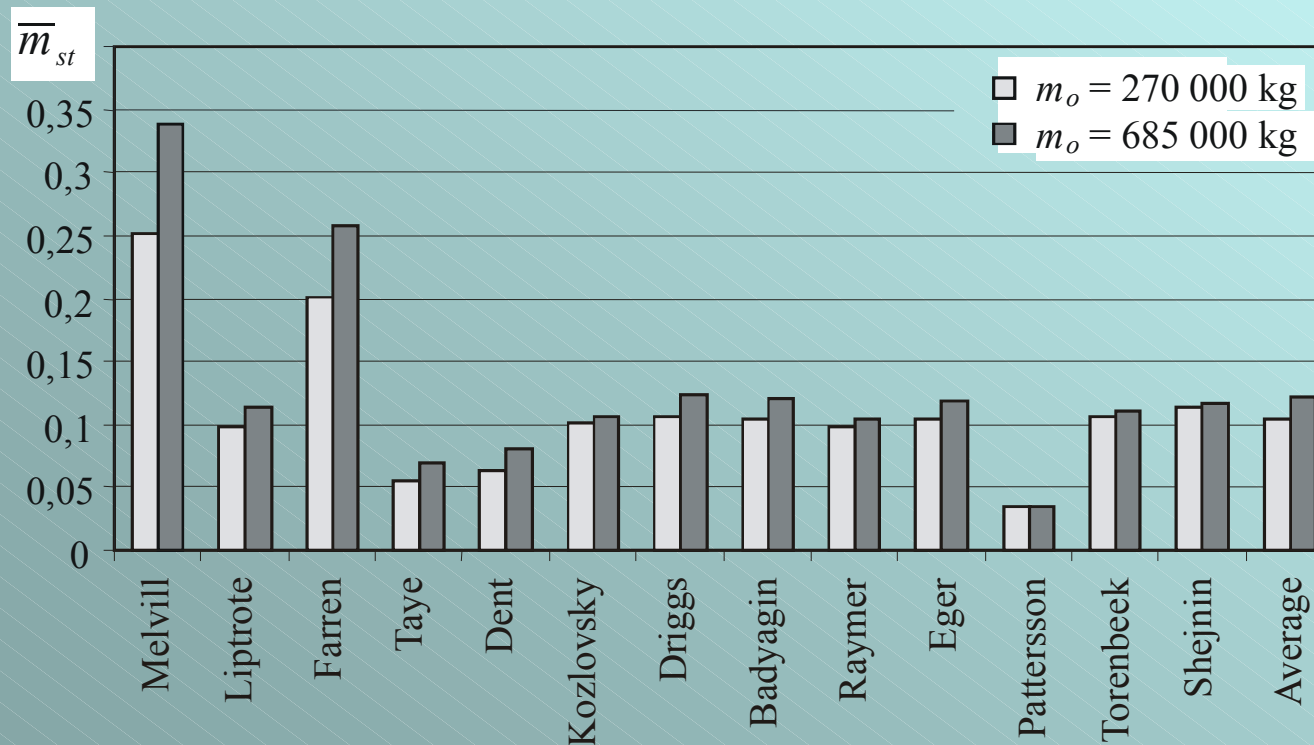
$$\bar{m}_{st} = \frac{m_{st}}{m_o}$$



# Example of calculation a wing mass fraction via “weight equation”

Typical weight equation (Eger)

$$\overline{m}_{st} = \frac{7k_1 n_p \phi \lambda \sqrt{m_0}}{10^4 p_0 (\overline{c_0})^{0,75} \cos^{1,5} \chi} * \frac{\eta + 4}{\eta + 1} * \left( 1 - \frac{\mu - 1}{\eta + 3} \right) + \frac{4,5k_2 k_3}{p_0} + 0,015$$



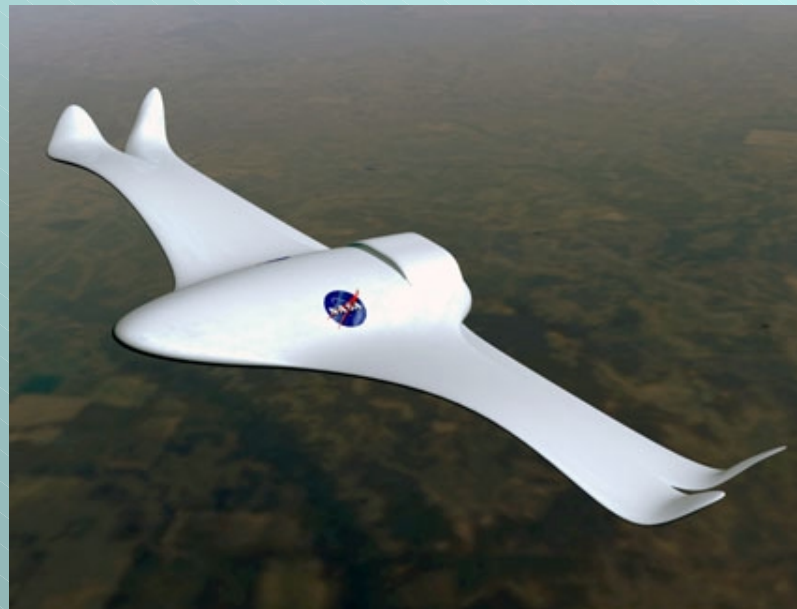


## **Weight Check**

1. Definition of the weight limits for different part of structure before design.
2. Analyses of weight penalty after design (if necessary).  
Looking for decrease of structural mass.

# Unconventional flight vehicles

Morphing Wing from TUDelft



(<http://www.lr.tudelft.nl/live/pagina.jsp?id=fd5540a7-0cfe-44e5-b1bc-c806fa0410b8&lang=en> )

$$m_{st} = ? \quad \overline{m}_{st} = ??$$

## New ideas for improving design process

1<sup>st</sup> idea. Load-carrying factor

Frame 
$$G = \sum_{i=1}^n |N_i| \cdot l_i$$

Thin-wall structure 
$$G = \sum_{i=1}^n R_i \cdot S_i$$

3D-structure 
$$G = \int_V \sigma^{eqv} dV$$



## Definition of structural mass via “load-carrying factor”

Theoretical structural material volume

$$V_T = \sum_{i=1}^n \frac{|N_i|}{[\sigma]} \cdot l_i = \sum_{i=1}^n F_i \cdot l_i$$

Real mass of structure

$$m_{st} = \varphi \cdot \rho \cdot V_T = \varphi \cdot \rho \cdot \frac{G}{[\sigma]} \quad \text{or} \quad m_{st} = \varphi \frac{G}{\bar{\sigma}}$$

$G$  – take into account topology, geometry and external loads

$\bar{\sigma}$  – specific durability of material

$\varphi$  – coefficient of full-mass structure, (it depends on design and technology perfect)

**G-criteria allows to calculate absolutely mass of unconventional structure with high accuracy**



2<sup>nd</sup> idea. Size less criteria of load carrying  
perfection of structure

***Load-carrying factor*** is proportional to the linear  
sizes (coordinates of nodals) of structure and  
value of nodal forces (at retaining of the law of  
distribution of external loading) –  
***dimensional quantity***

**Sizeless criteria– coefficient of load carrying  
factor**

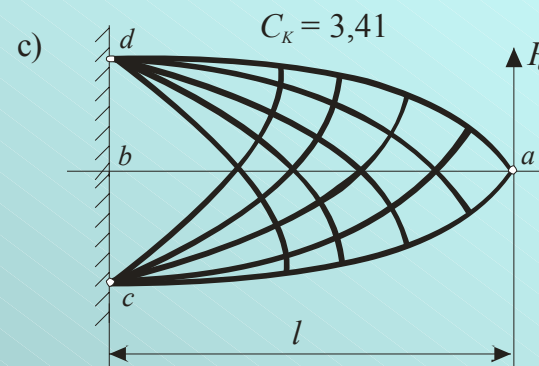
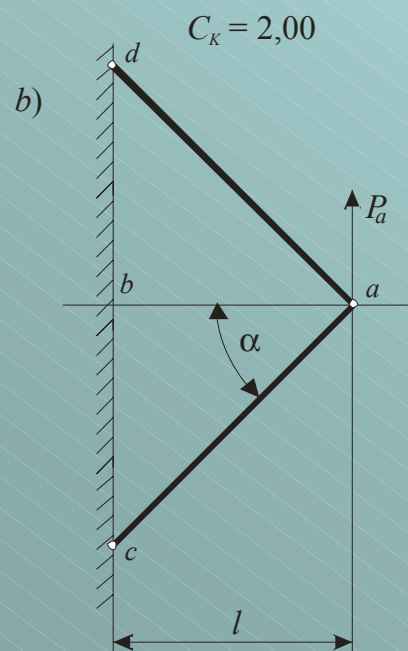
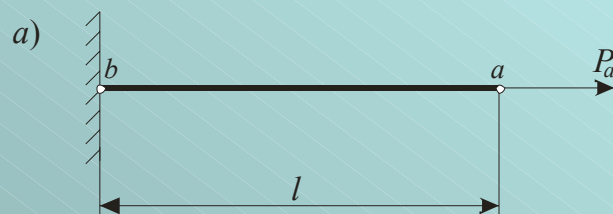
$$C_K = \frac{G}{P \cdot L}$$

*where P- specific load  
L- specific size*

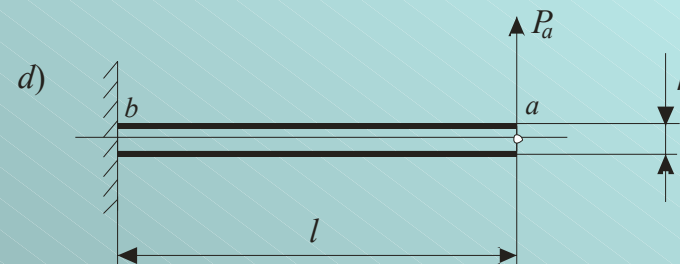
whence  $G = C_K PL$  (aerodynamic analogy :  $Y = C_y qS$  )

## Example of simple structures

$$C_K = 1,00$$



$$C_K = 10,00$$





## New weight equation for definition of full wing mass and wing mass fraction

Specific size – square of wing in degree  $\frac{1}{2}$  -  $\sqrt{S}$

Specific load – lift  $Y = n \cdot m_o \cdot g$

$$G = C_K \cdot n \cdot m_o \cdot g \cdot \sqrt{S}$$

whence

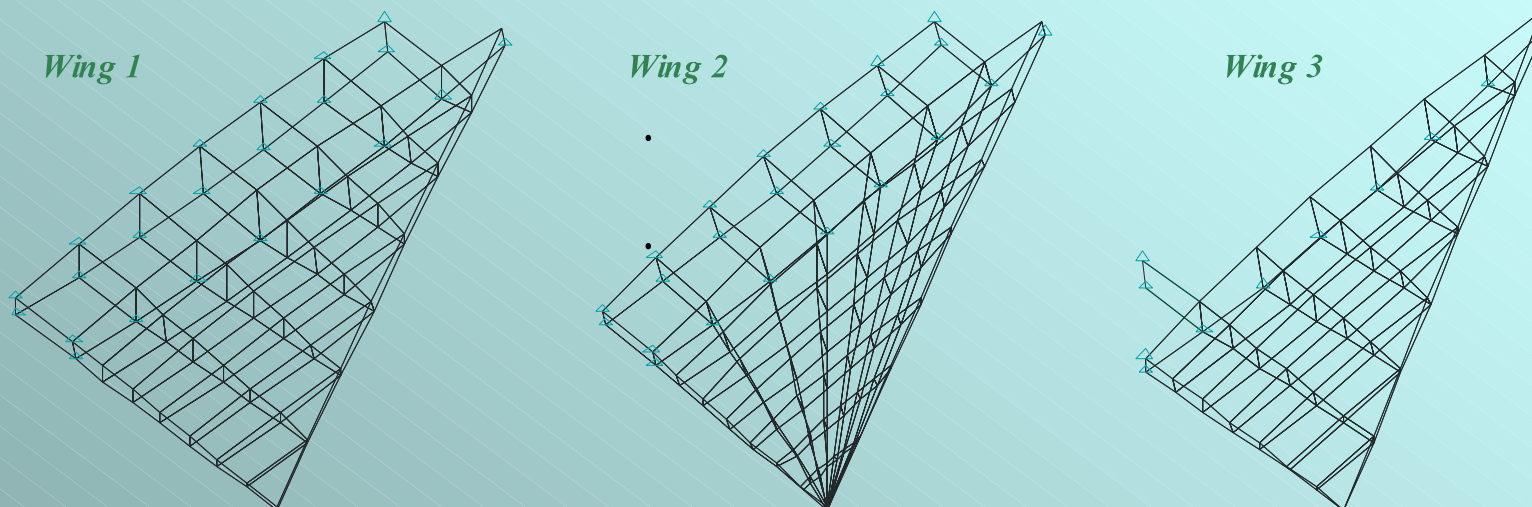
$$C_K = \frac{G^*}{n^* \cdot m_o^* \cdot g \cdot \sqrt{S^*}}$$

**Weight equation :**

$$\overline{m}_{wing} = \frac{\varphi}{\overline{\sigma}} C_K \cdot n \cdot g \cdot \sqrt{S} \quad m_{wing} = \frac{\varphi}{\overline{\sigma}} C_K \cdot n \cdot m_o \cdot g \cdot \sqrt{S}$$

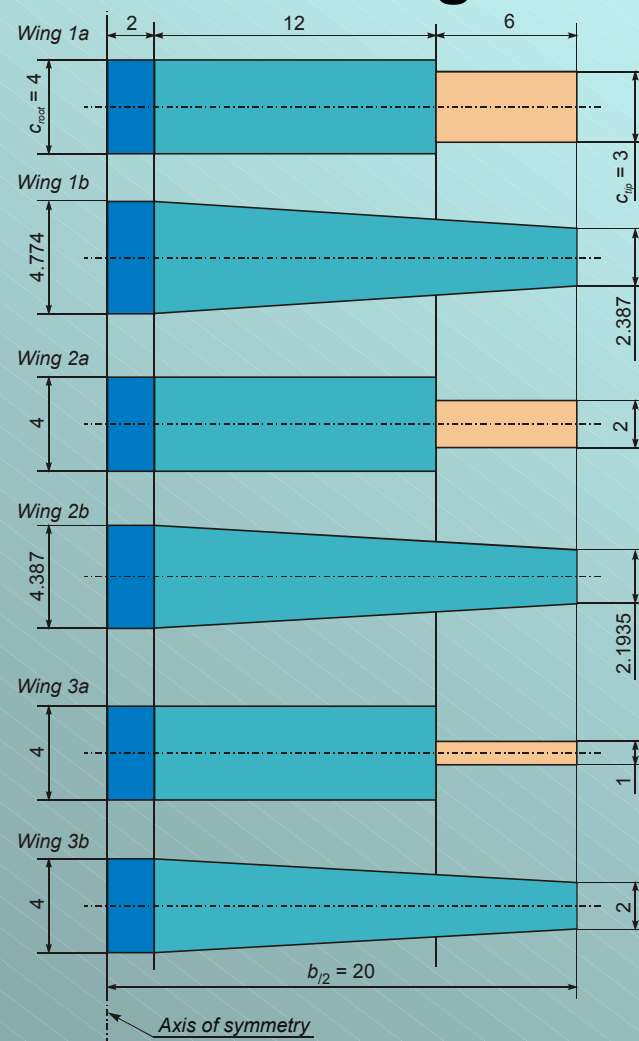


## Example of structural topology choice



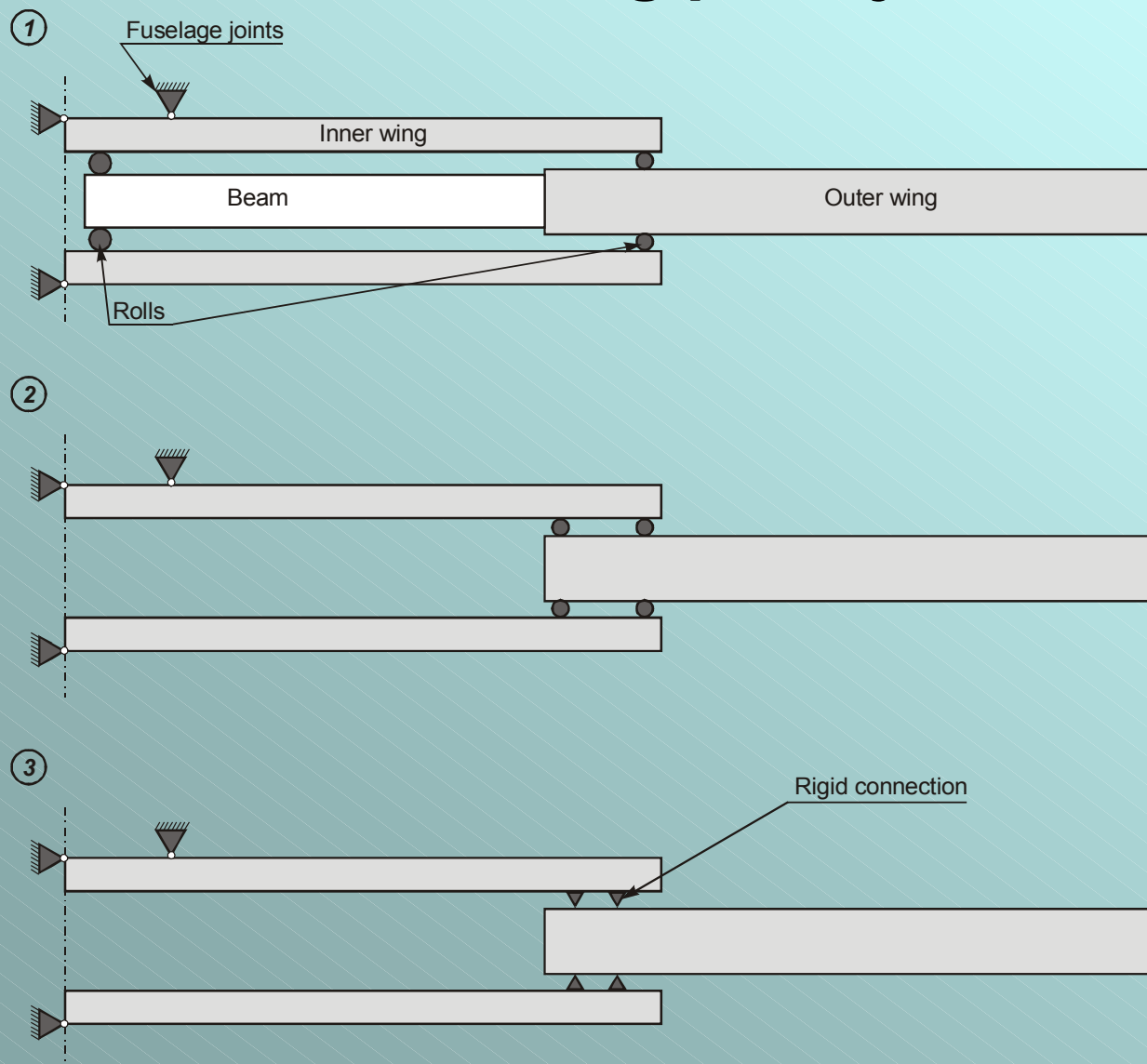
Wing	Membrane structures	Panel structures					
		Strategy I			Strategy II		
		$\bar{\delta} = 0,6$	$\bar{\delta} = 0,5$	$\bar{\delta} = 0,4$	$\bar{\delta} = 0,6$	$\bar{\delta} = 0,5$	$\bar{\delta} = 0,4$
1	1,62	1,68	1,70	1,71	1,84	1,94	2,07
2	1,68	1,76	1,78	1,81	1,83	1,89	1,98
3	2,55	2,69	2,75	2,83	2,68	3,03	3,56

## Example of morphing wing aerodynamic and weight efficiency research



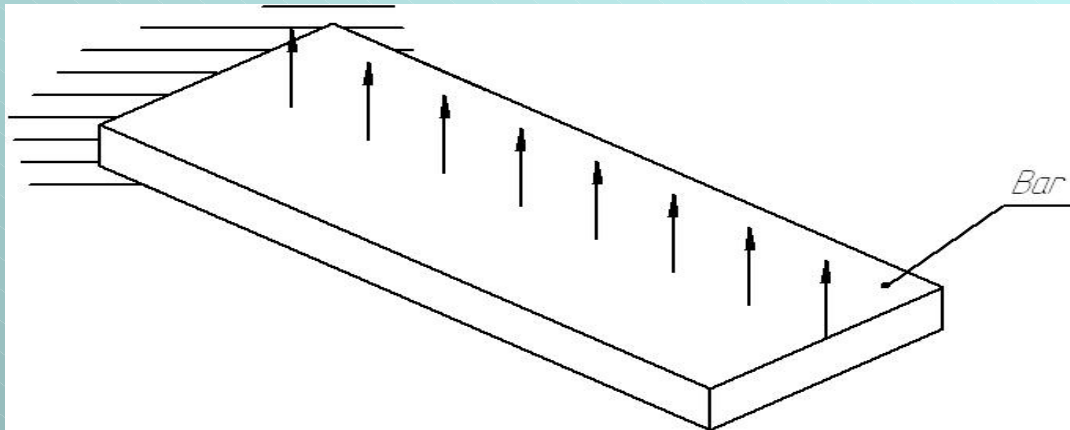
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## Scheme of wing parts joints

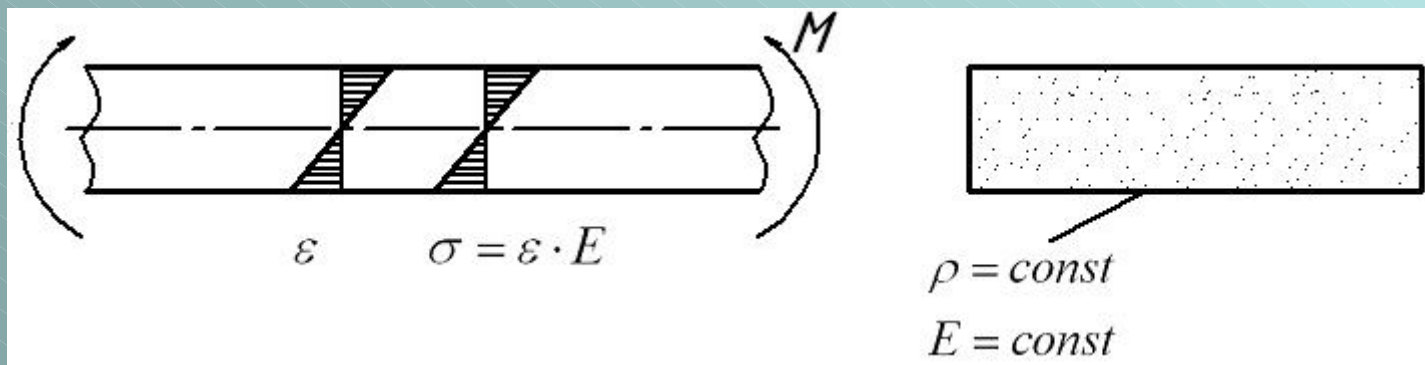


### 3<sup>rd</sup> idea. Using 3D-model with variable density

Model



Traditional material



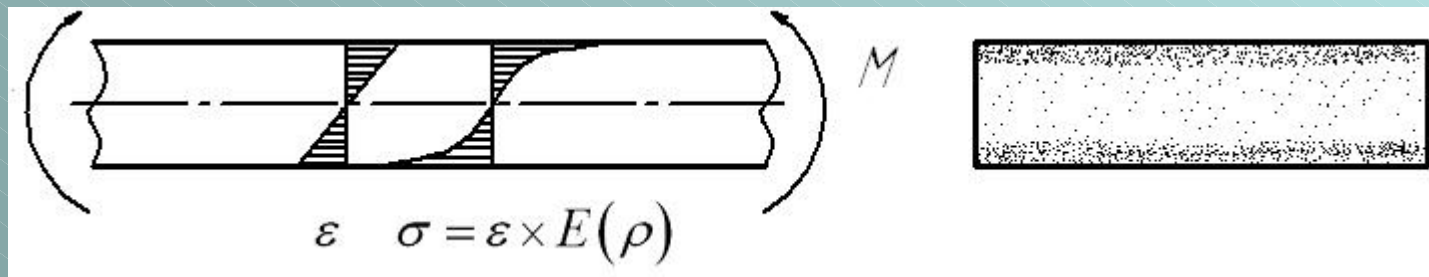
Hypothetic material with variable density

$$[\sigma] = \rho \cdot [\bar{\sigma}]$$

$$E = \rho \cdot \bar{E}$$

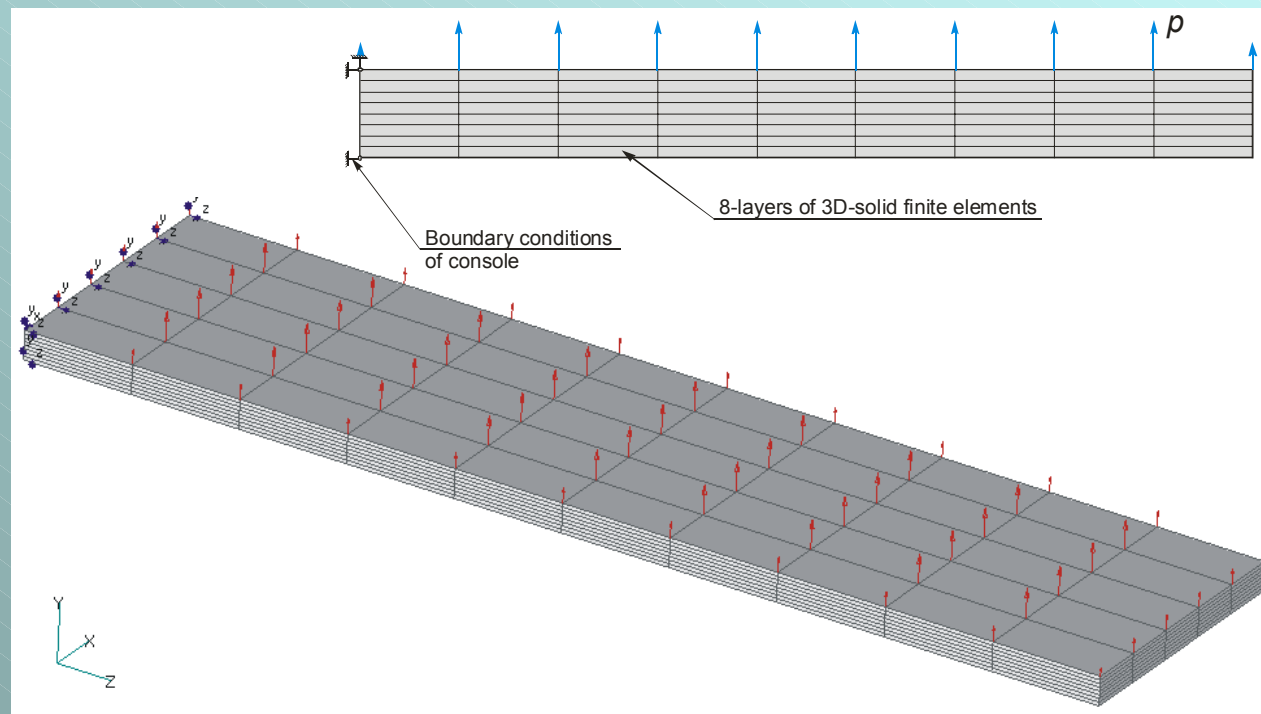
Algorithm of density distribution optimization

1.  $\rho_{0i} = \text{const}$
2.  $\sigma_i$
3.  $\rho_{1i} = \sigma_{0i}^{eqv} / [\bar{\sigma}]$



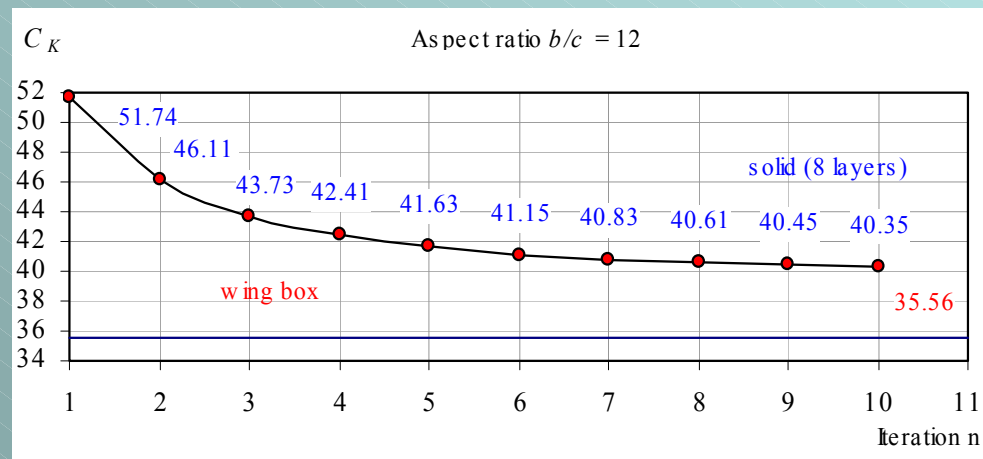
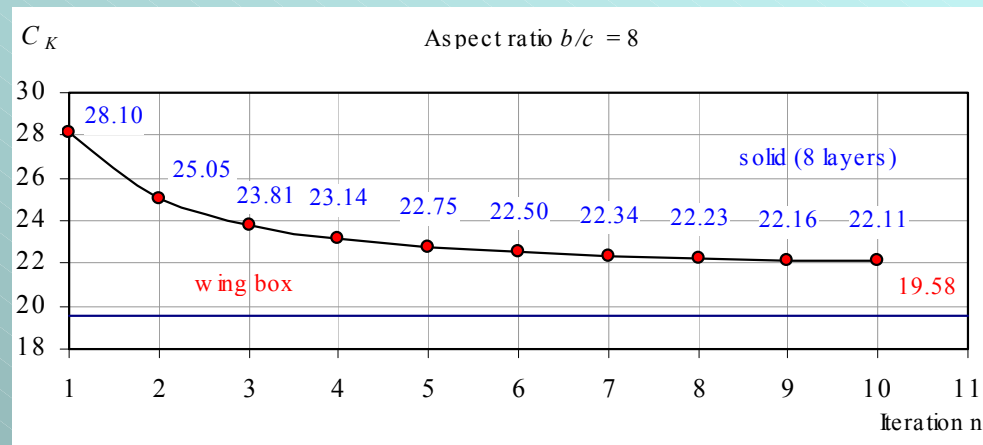
## Test

### 3D-model of the wing structure





## Comparison of load-carrying factor coefficient calculations for thin-wall structure and 3D-solid model with variable density

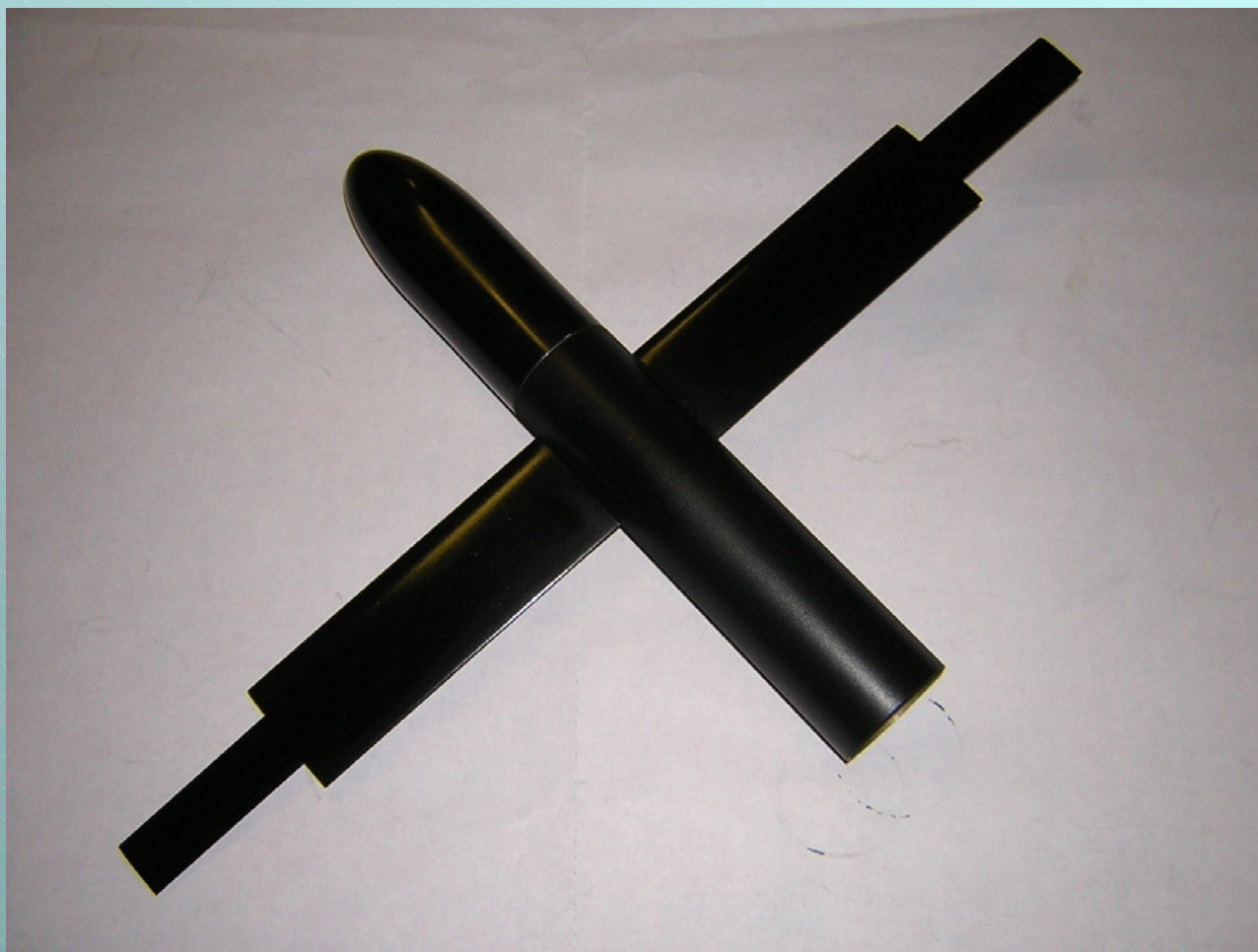






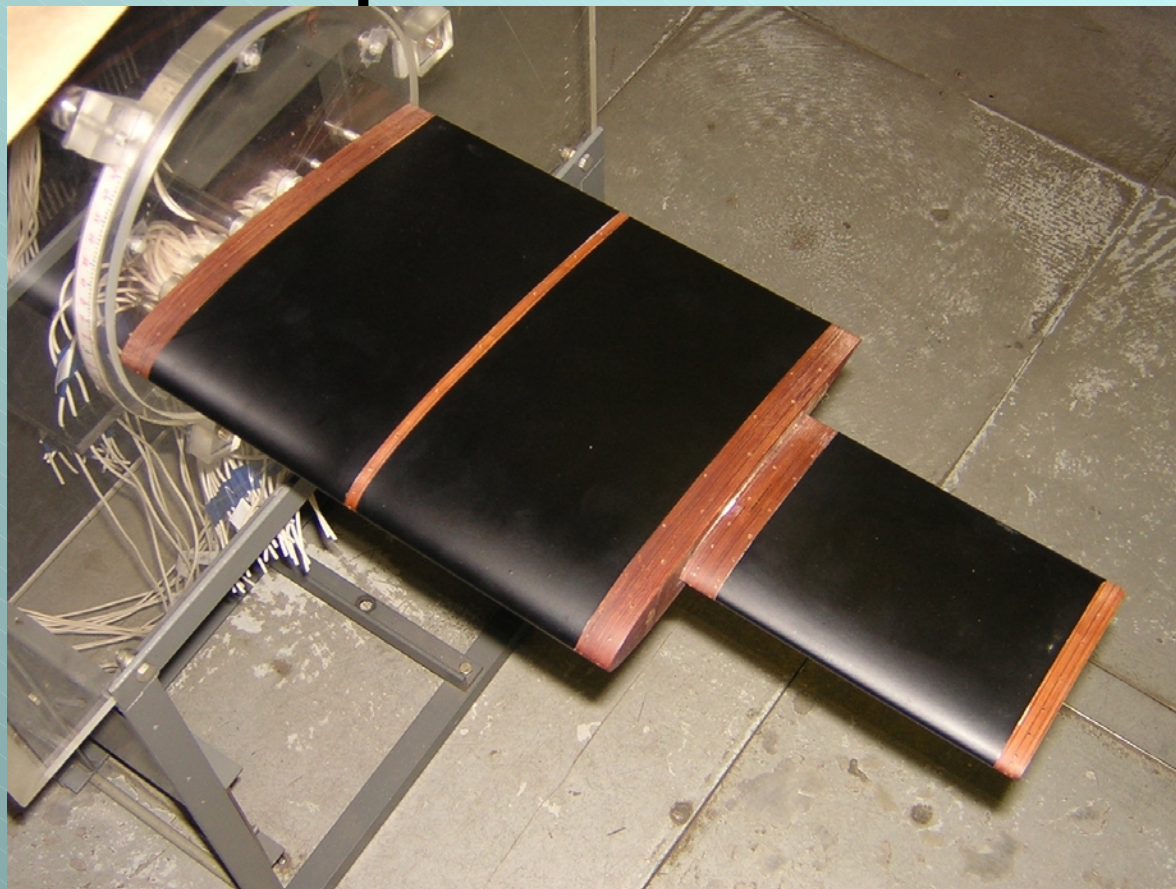
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## **Wind tunnel model 1**

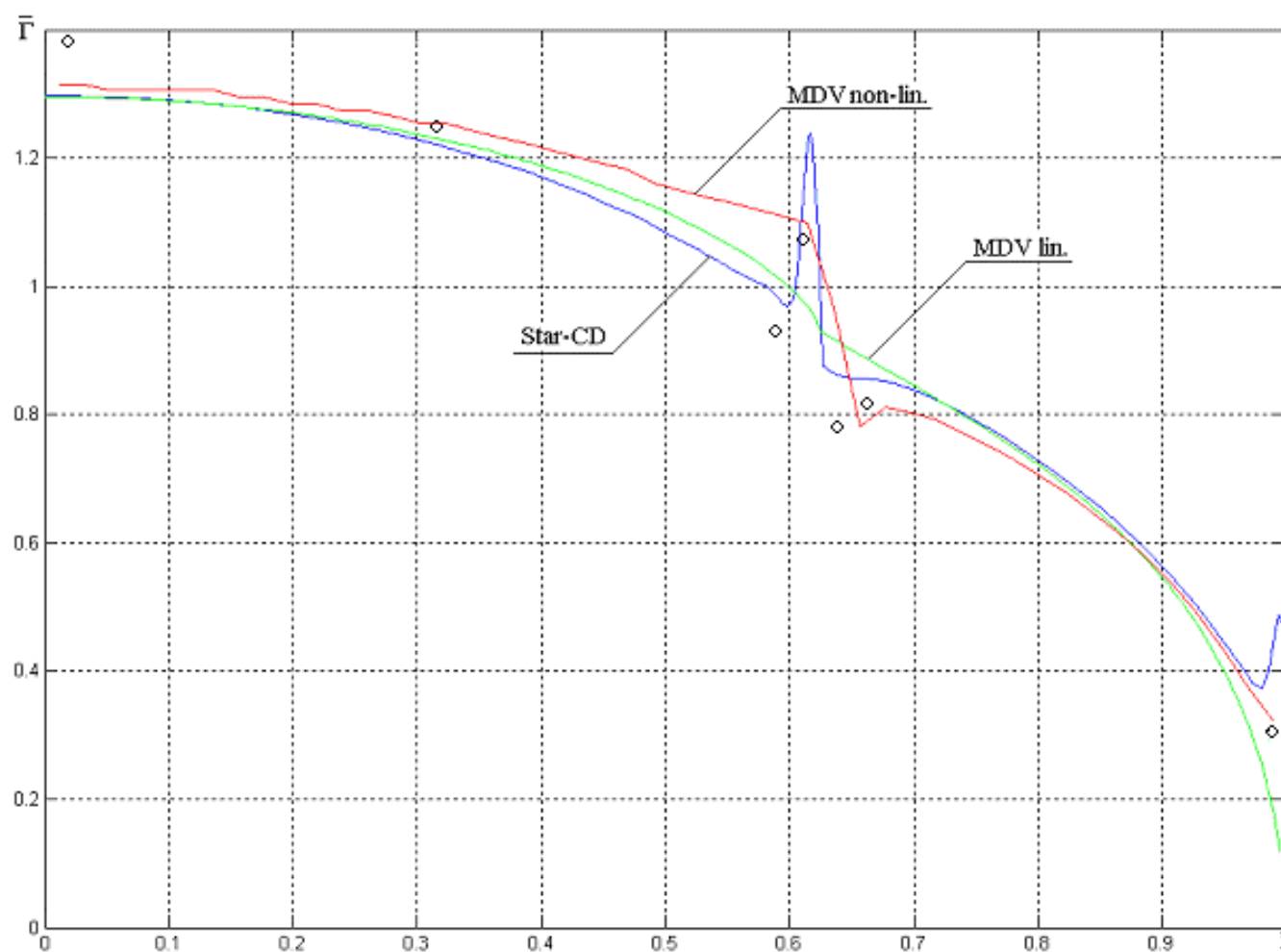




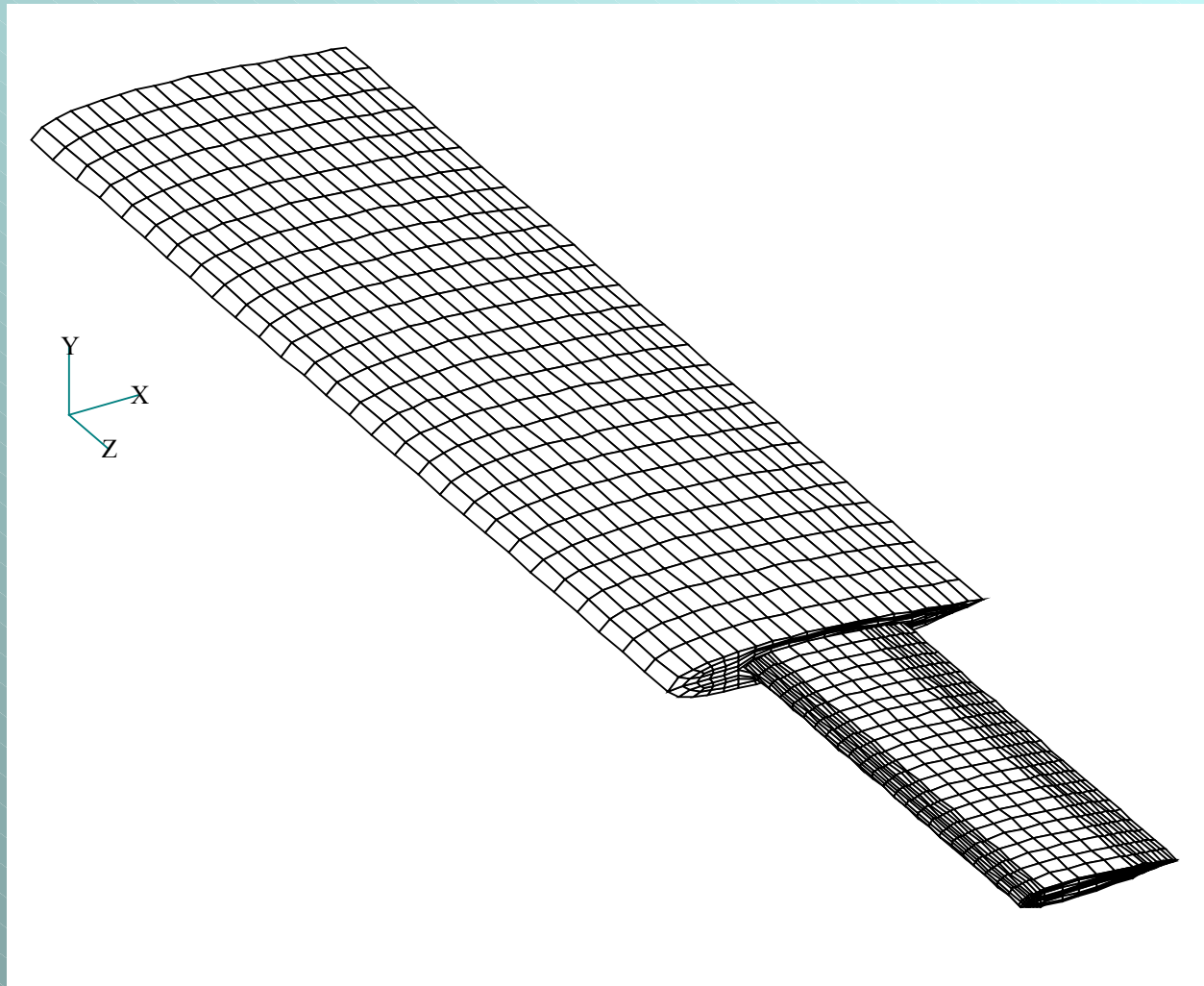
## Wind tunnel model 2 with pressure of orifices



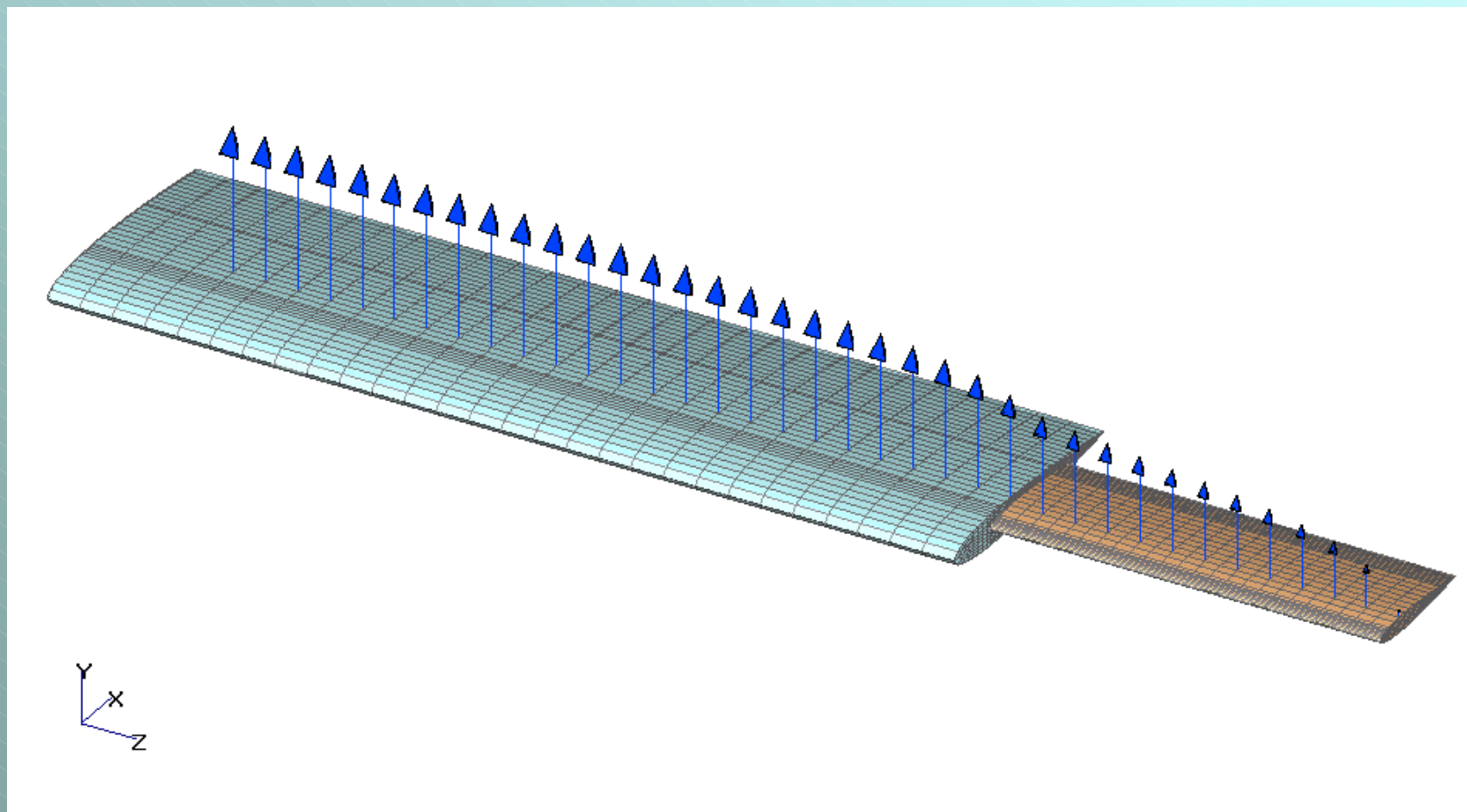
## Spanwise load distributions



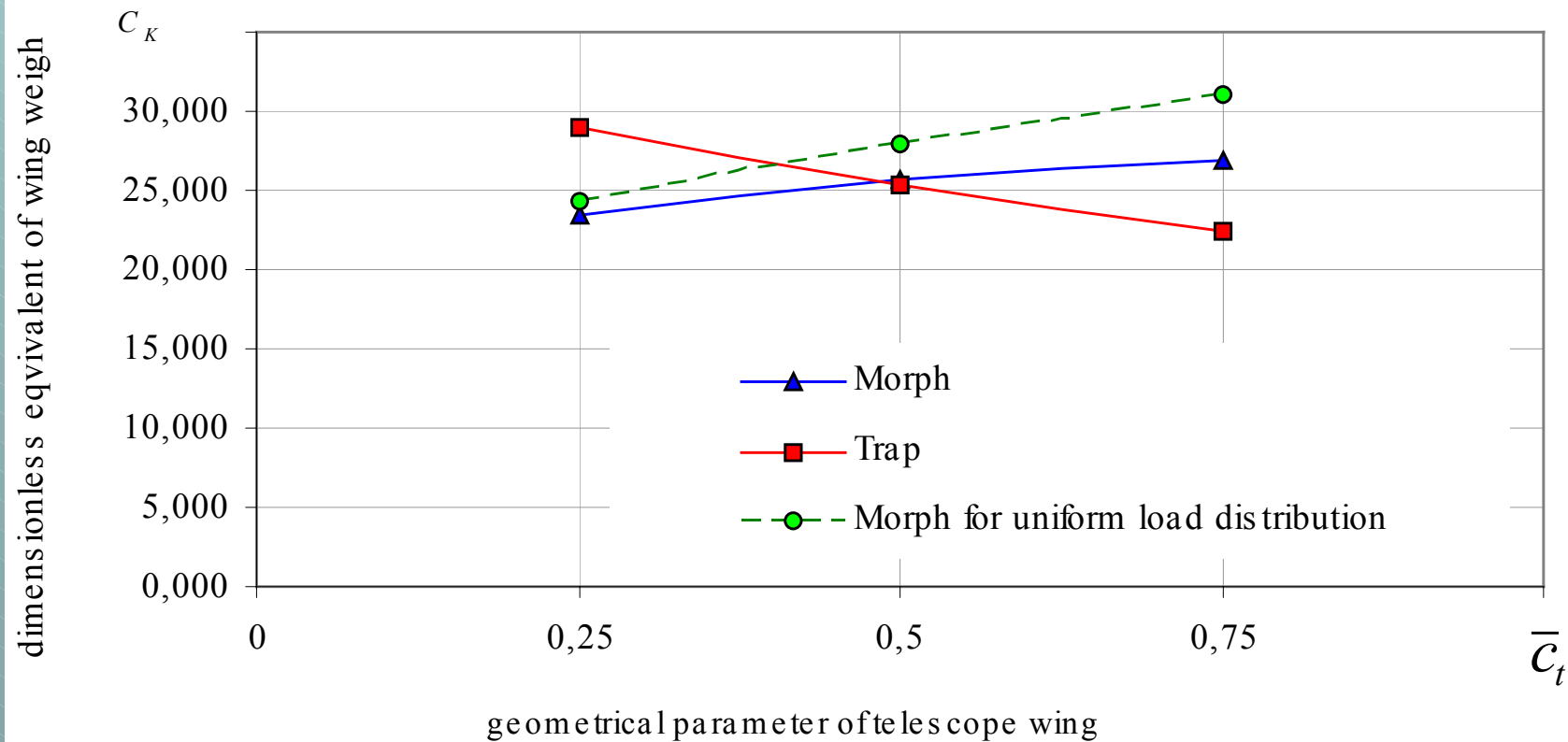
## 3D-model with variable density of material



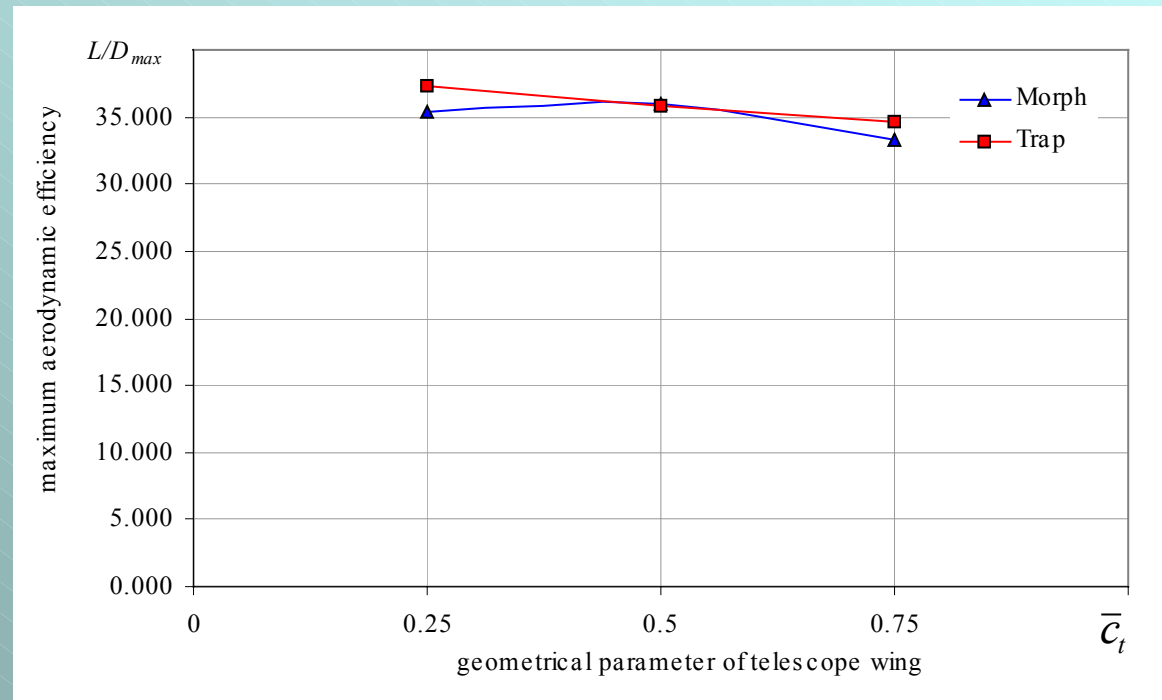
## External loads



## Comparison of weight perfection



## Comparison maximum aerodynamic efficiency







## Pressurized cabin, pressure vessel

Specific volume – volume -  $V$

Specific load– pressure –  $P$

$$C_K = \frac{G}{P \cdot V}$$

Some results for reservoirs:

Spherical –  $C_K = \frac{3}{2}$

Cylindrical –  $C_K = \sqrt{3}$

Spherical from CM –  $C_K = 3$

Cylindrical from CM –  $C_K = 3$

## Conclusion

***Load-carrying factor  $C_K$  allows:***

1. To put in according to load-carrying scheme (topology of structure) the certain dimensionless value which defines weight perfection of a design.
2. To build "weight" formulas for any designs.
3. To accumulate the knowledge in convenient form (dimensionless!) for analysis of existing and perspective designs.

There are 3 new ideas in the lecture, which can be useful to increase efficiency of early stage design.